

# S-CO<sub>2</sub> Brayton Loop Transient Modeling

The 4<sup>th</sup> International Symposium on  
Supercritical CO<sub>2</sub> Power Cycles

September 9 & 10, 2014

MATRIX Style RECUPERATOR M  
Core 56.4" L x 16.4" H x 7.1" W (w/o  
FLUID = CO<sub>2</sub>. Effective HXA = 633 ft<sup>2</sup> (based on 4  
Flow Area set at 0.1306 ft<sup>2</sup> for the Hot LP and  
8,704 LPchannels (Dh=0.0465"), 8,704 HPchan  
Hot CO<sub>2</sub> Flow Rate 12.03 lb/s (4.330  
Cold CO<sub>2</sub> Flow Rate 12.21 lb/s (4.35  
Design Heat Load = 1459 kW, HB

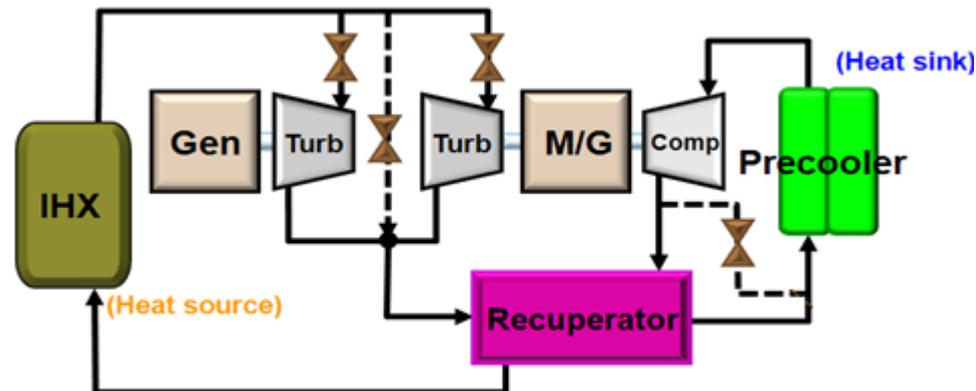
# Outline

- Background
- Model Results and Comparisons with Test Data
  - Steady State Heat Balance
  - Transient
    - Turbomachinery Start-up
    - Power Transients
- Next Steps/Model Updates
  - NIST REFPROP/FIT
  - Test data
- Summary

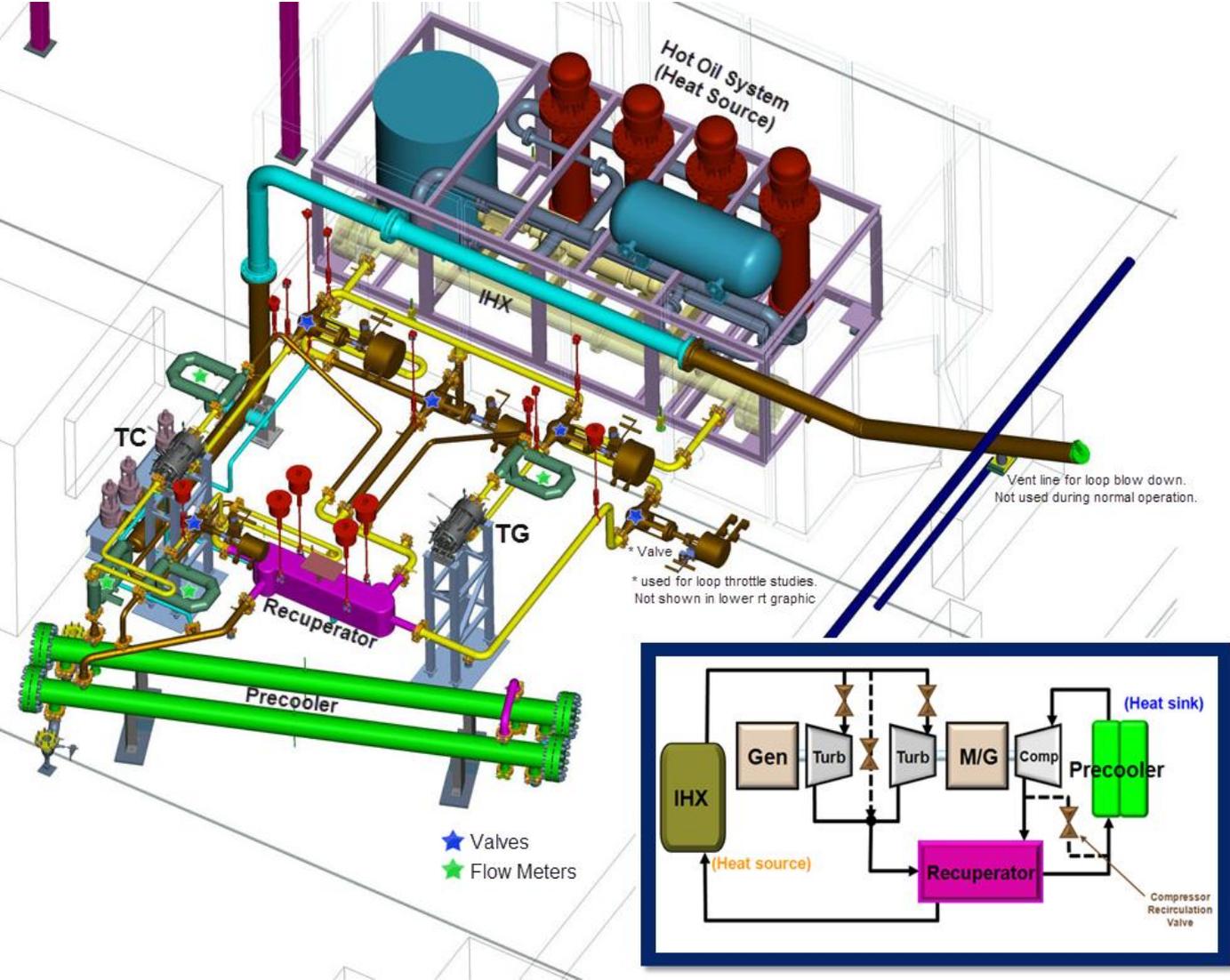
# Background

## ➤ Integrated Systems Test (IST)

- Characteristics
  - Recuperated Closed Cycle Brayton
  - Rated power 100kWe
  - Power and Compressor Turbines in Parallel
  - Constant Speed Turbine Generator
  - Generated power  $\propto$  Compressor Speed
  - Fixed inventory
- Purpose
  - Operational experience
  - Demonstrate system control
  - Validate transient model



# Background: Integrated Systems Test



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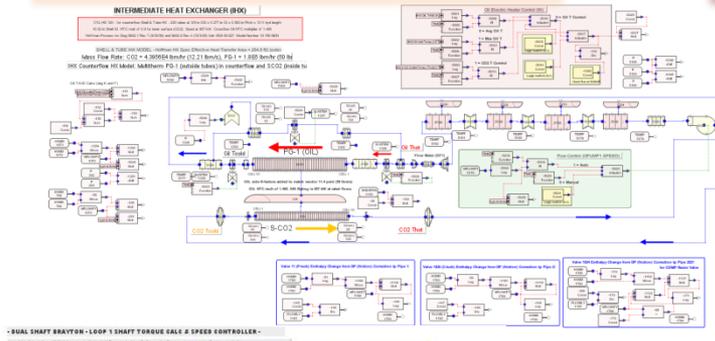


# Background: IST Transient Model

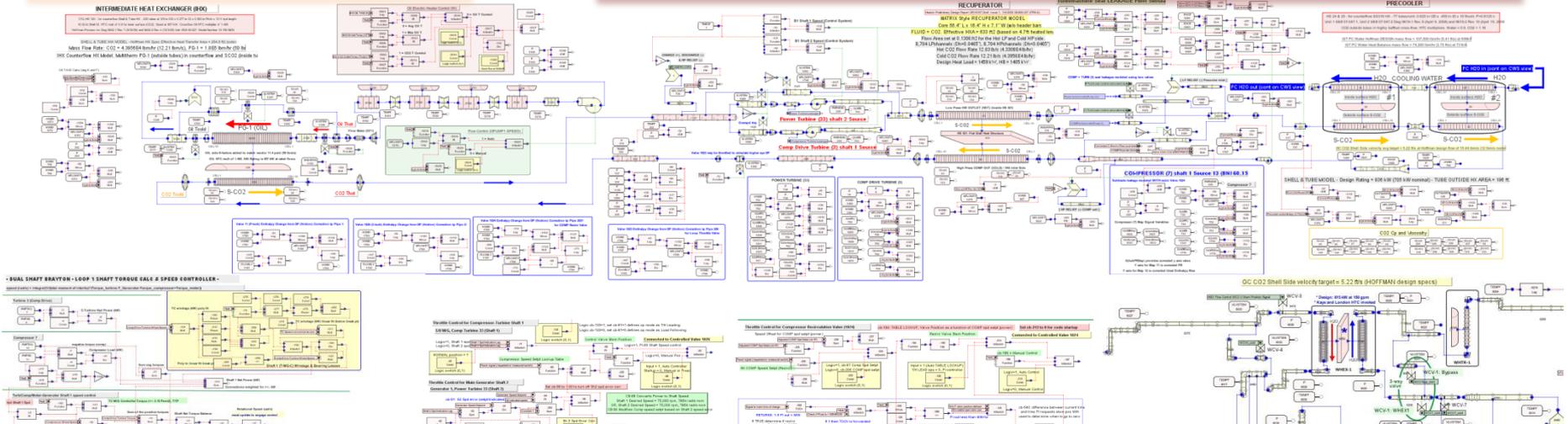
## ➤ IST Transient Model

- Built using TRACE and SNAP GUI
- Heat Source to Heat Sink
- Developed compressible fluid modeling methods
- Developed control systems

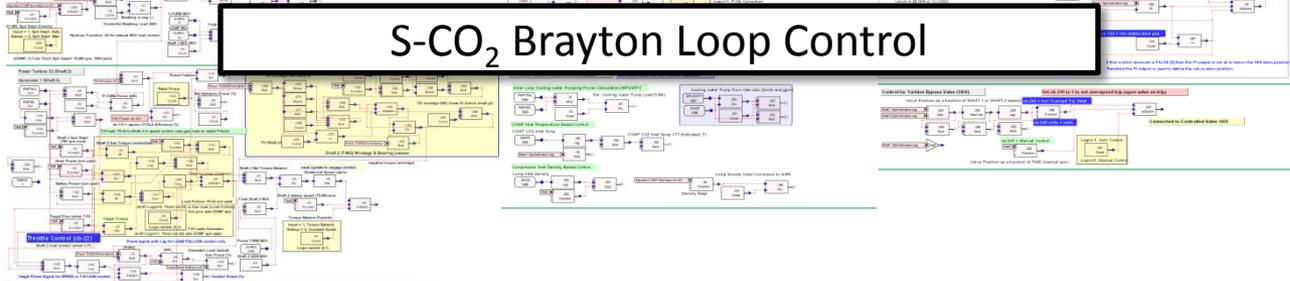
### Hot Oil System



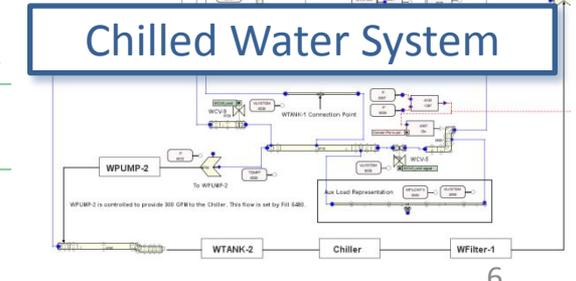
### S-CO<sub>2</sub> Brayton Loop



### S-CO<sub>2</sub> Brayton Loop Control

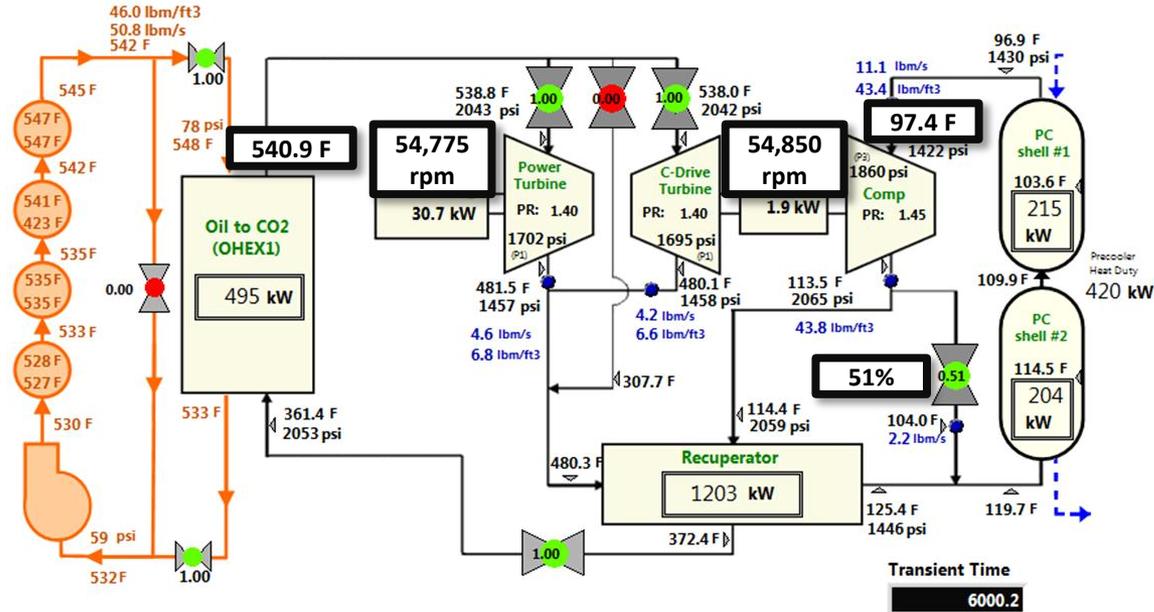


### Chilled Water System

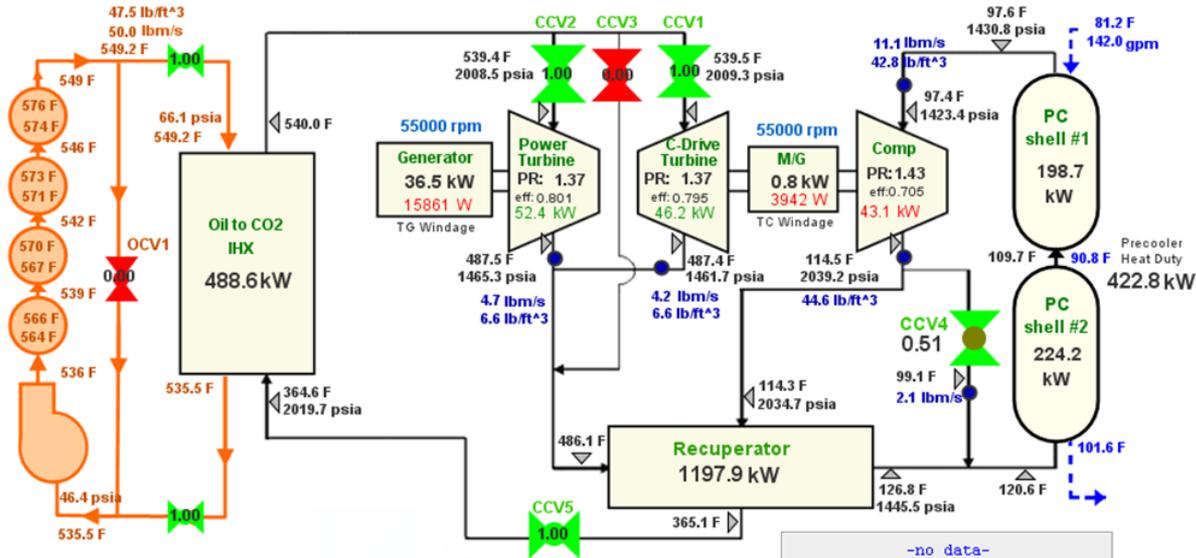


# Steady State Comparison: Updated Model

Test

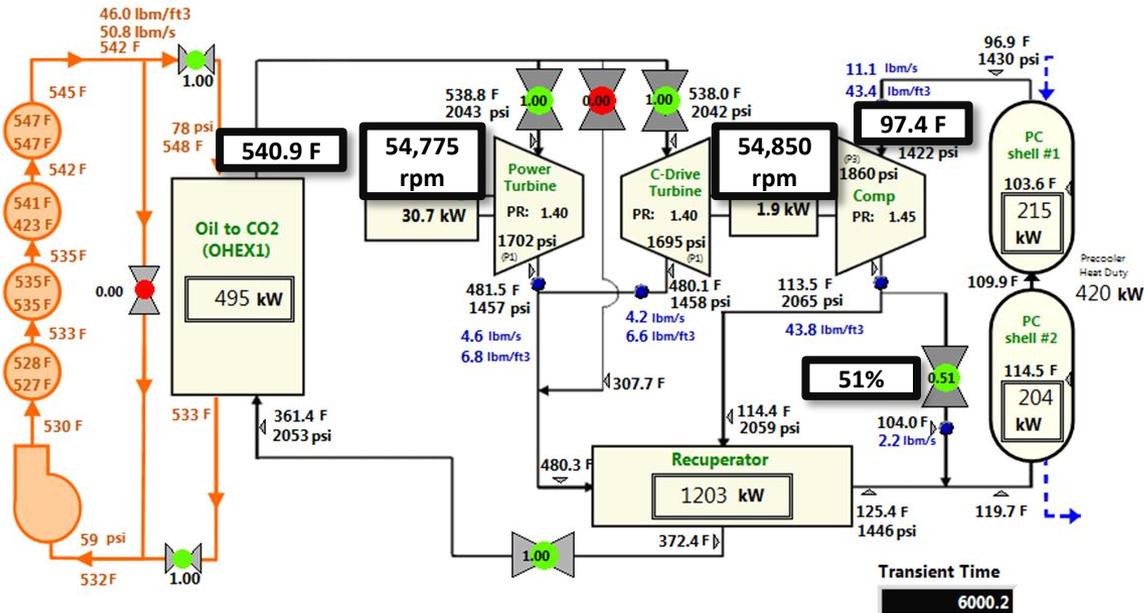


Model



# Steady State Comparison: Updated Model

Test



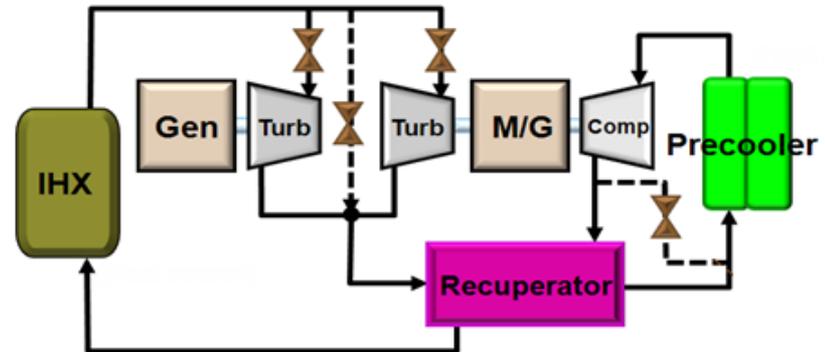
Parameter	Test	Pretest TRACE Model	TRACE Model With adjusted compressor map
Compressor Mass Flow (lbm/s) [kg/s]	11.1 [5.0]	10.1 [4.6]	11.1 [5.0]
Compressor PR	1.45	1.37	1.43
Compressor Exit Temperature (F) [K]	113.5 [318.3]	113.2 [318.1]	114.5 [318.8]

# IST Startup

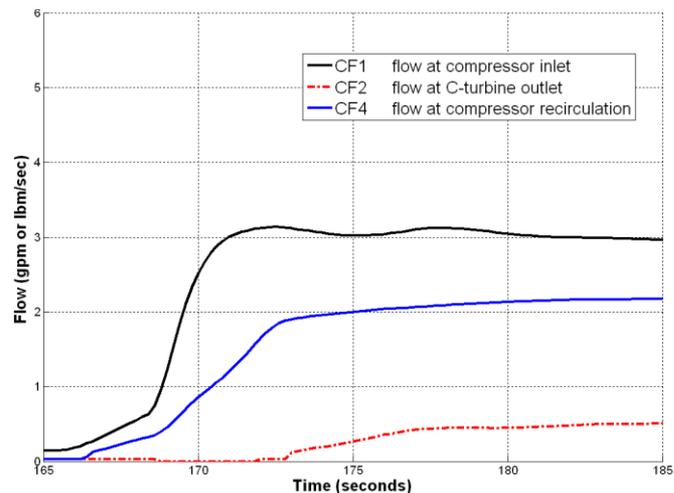
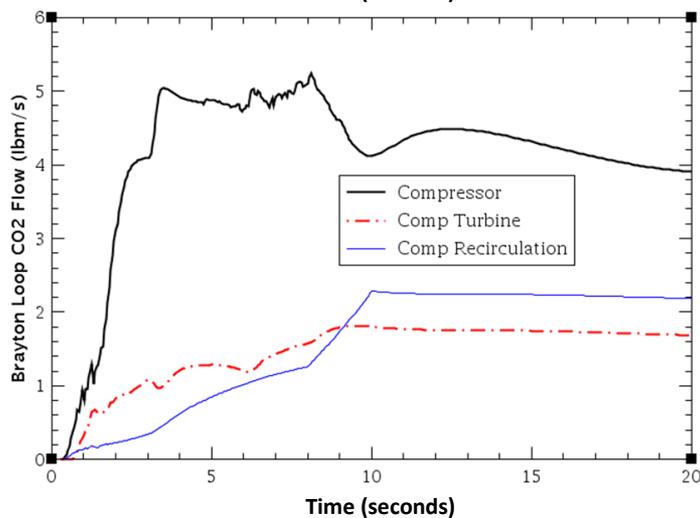
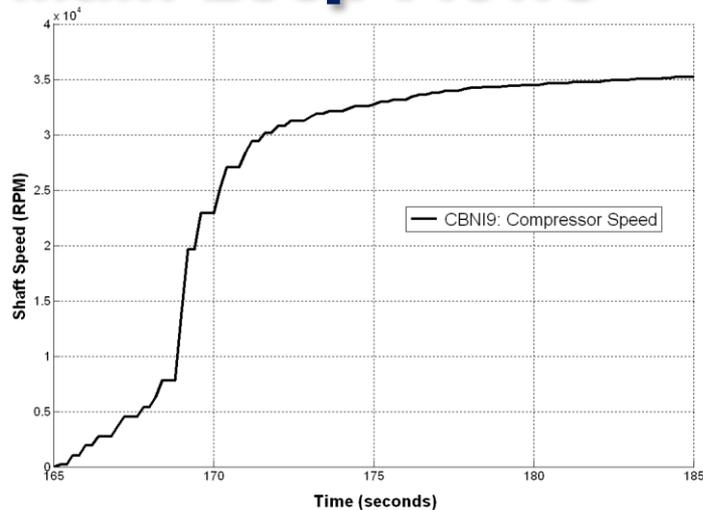
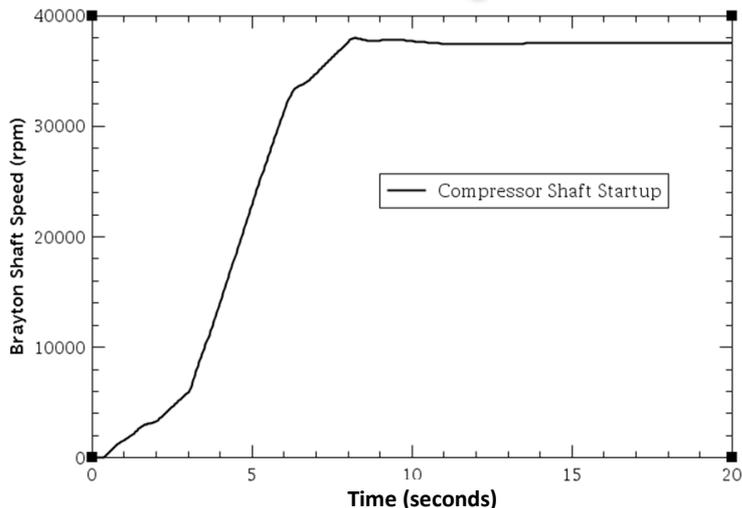
- Phenomenon considered during turbomachinery startup
  - Compressor surge
  - Reverse Turbine Flow
  - Gas Foil Bearing Lift-off

## Target Conditions for IST Turbomachinery Startup

Parameter	Target Value
Turbine inlet temperatures	165°F ( $Z = 0.7$ )
Compressor inlet temperature	100°F
Compressor inlet pressure	1230 psia
Turbine bypass valve	Shut
Compressor recirculation valve	83% open



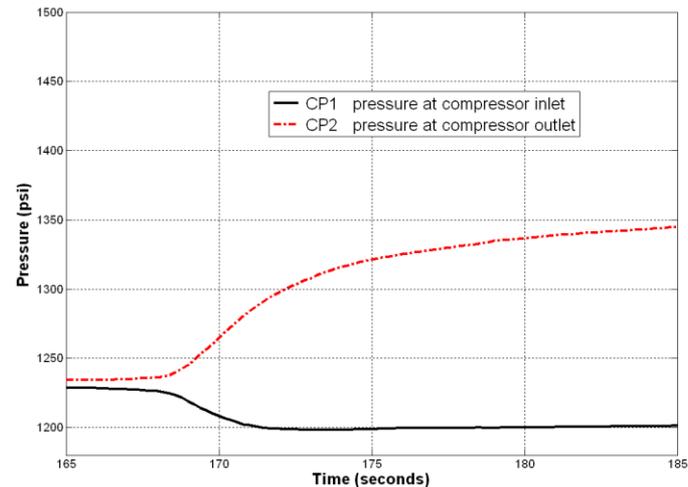
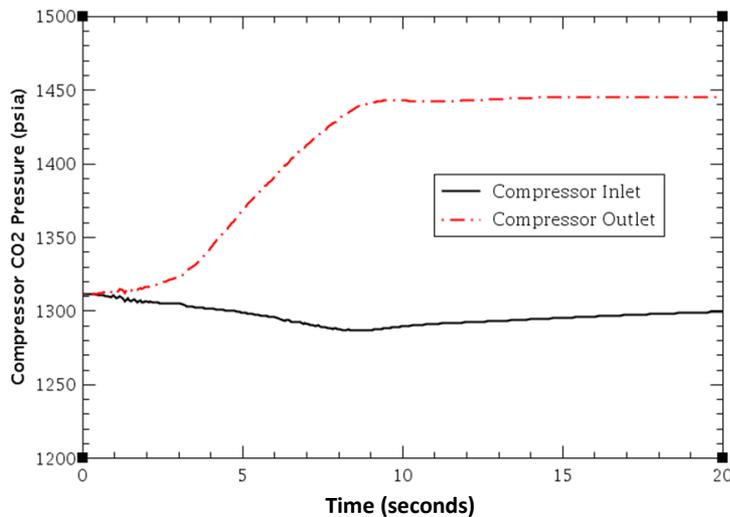
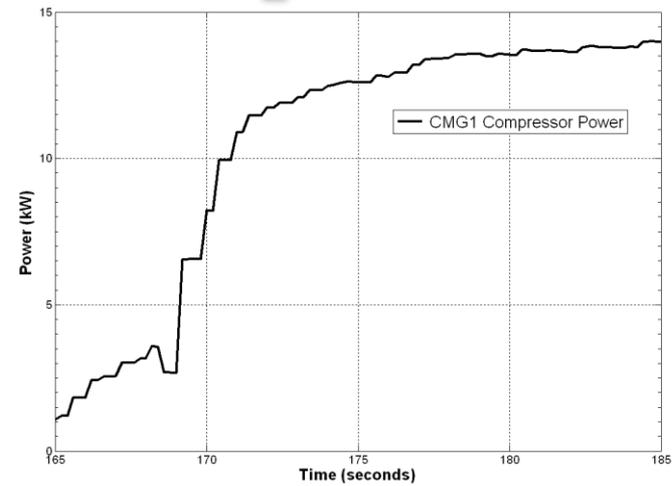
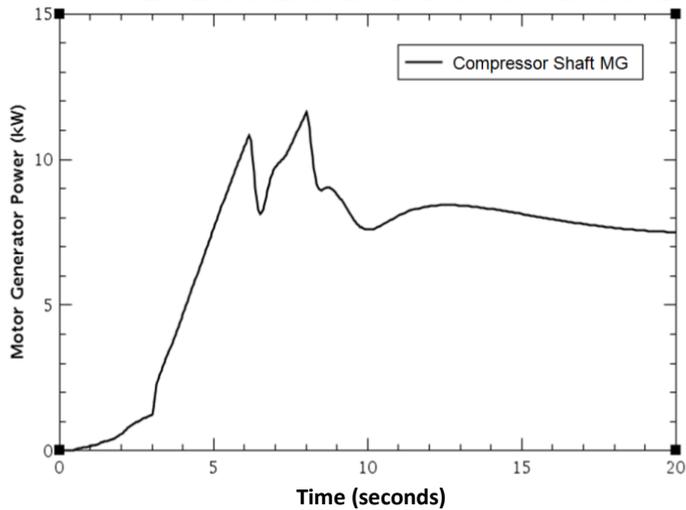
# IST Startup: Comparison between Model (left) and Test data (right) for Compressor Startup – Shaft Speed and Main Loop Flows



Model

Test

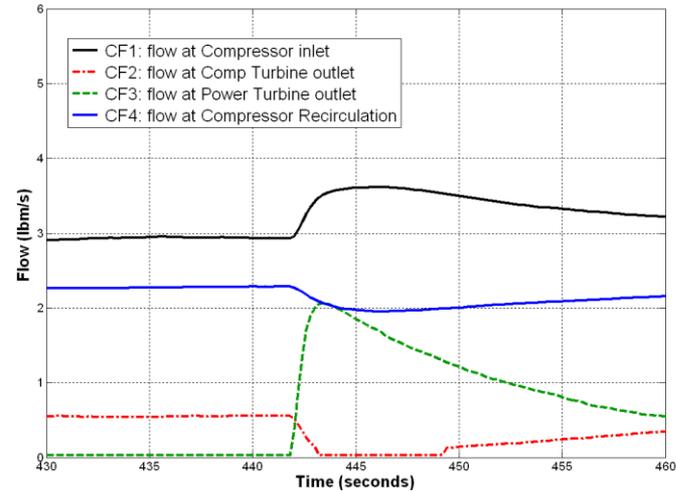
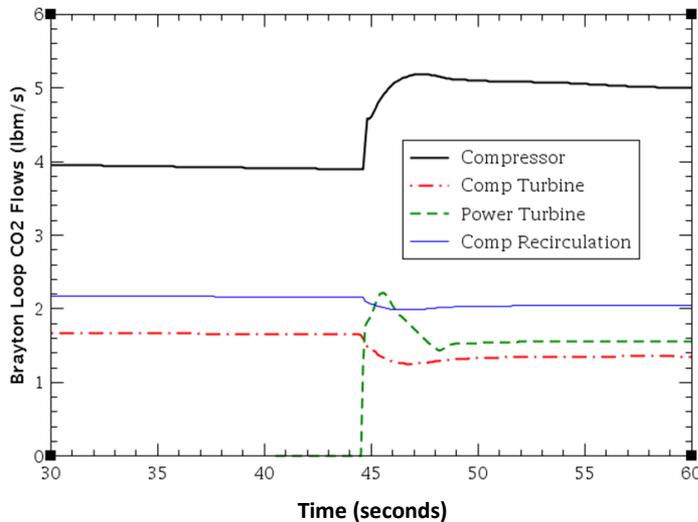
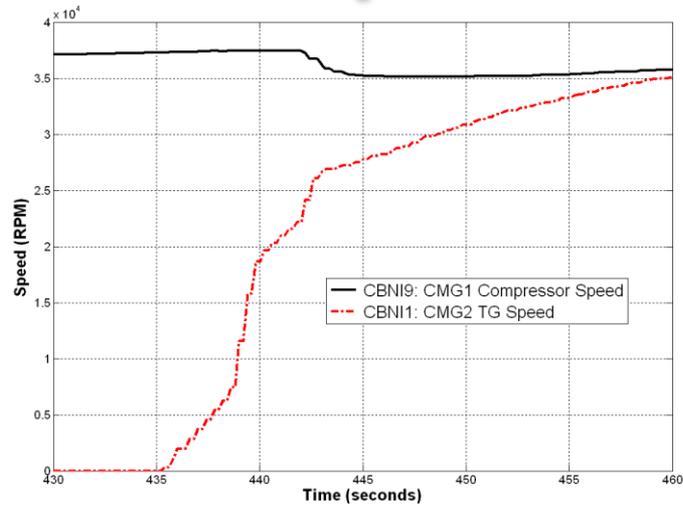
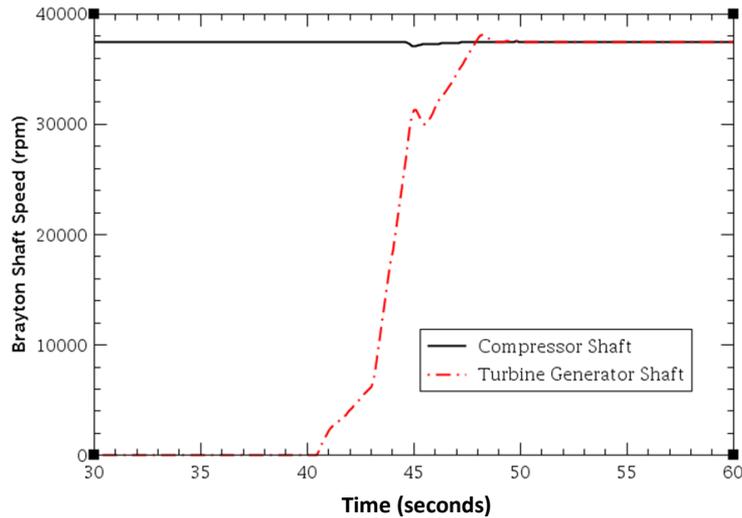
# IST Startup: Comparison between Model and Test for Turbine Compressor Startup – Shaft Motor Generator Powers and CO<sub>2</sub> Pressures



Model

Test

# IST Startup: Comparison between Model and Test for Turbine Generator Startup – Shaft Speed and Main Loop Flows



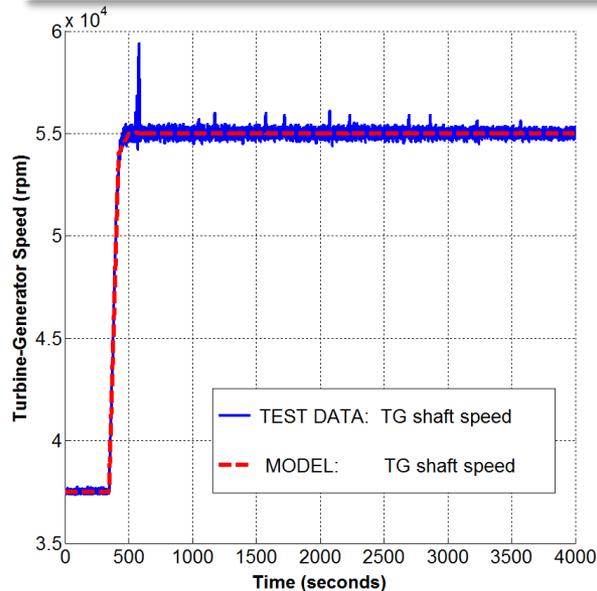
Model

Test

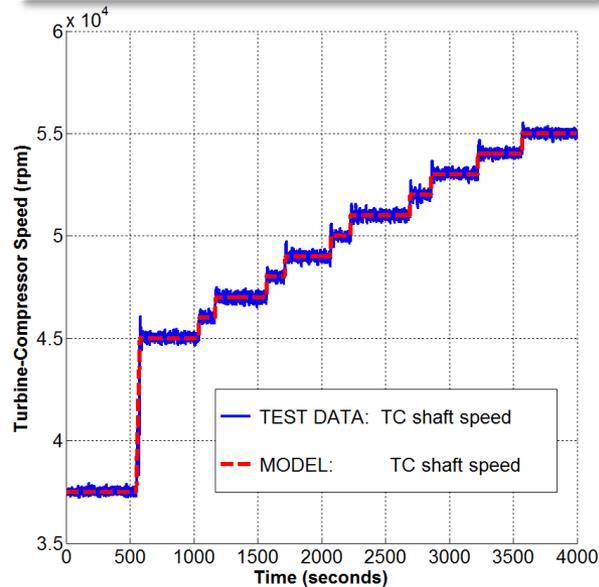
# Power Increase Transient

- Initial Conditions: Hot Idle (540°F/37,500 rpm)
- TG speed increased
- TC speed increased in steps
- Compressor recirculation valve decreased in steps
- Water flow automatically controlled to maintain compressor inlet T

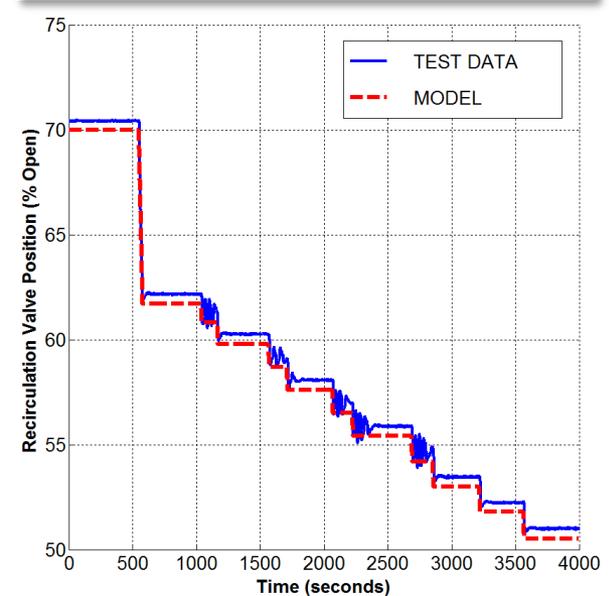
Turbine-Generator Speed



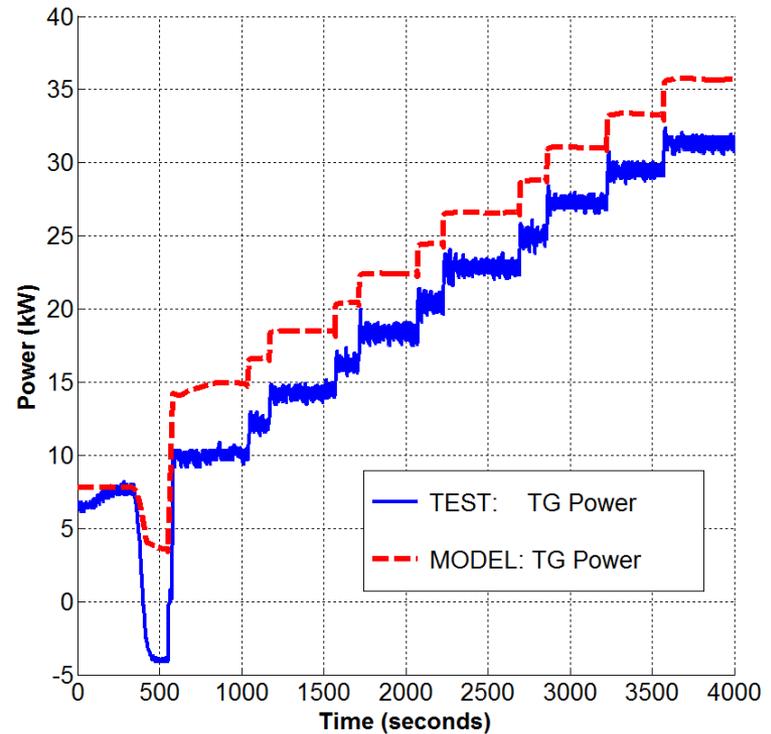
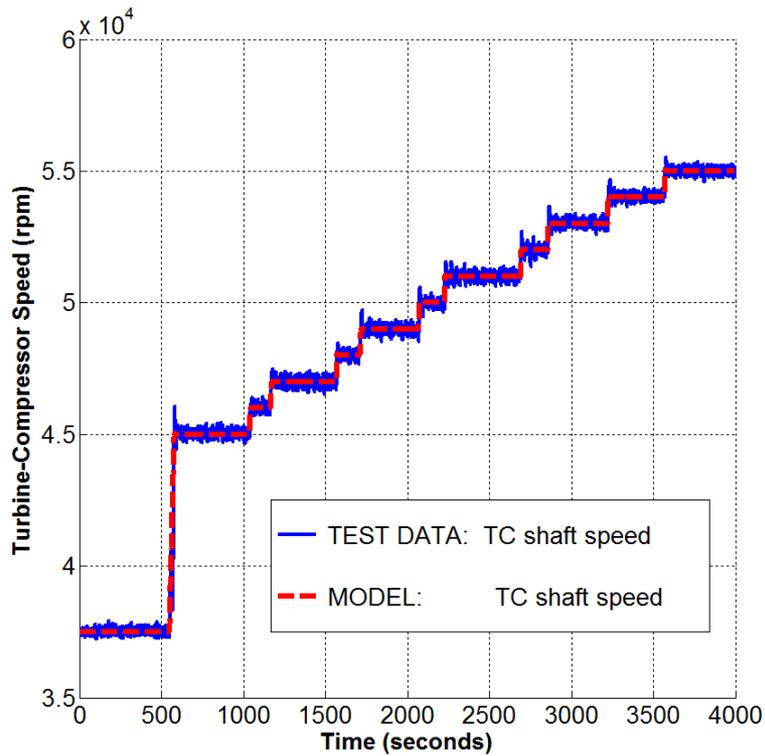
Turbine-Compressor Speed



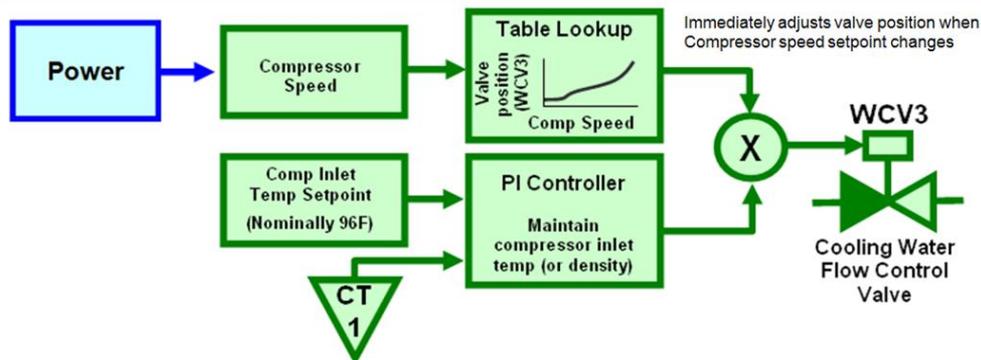
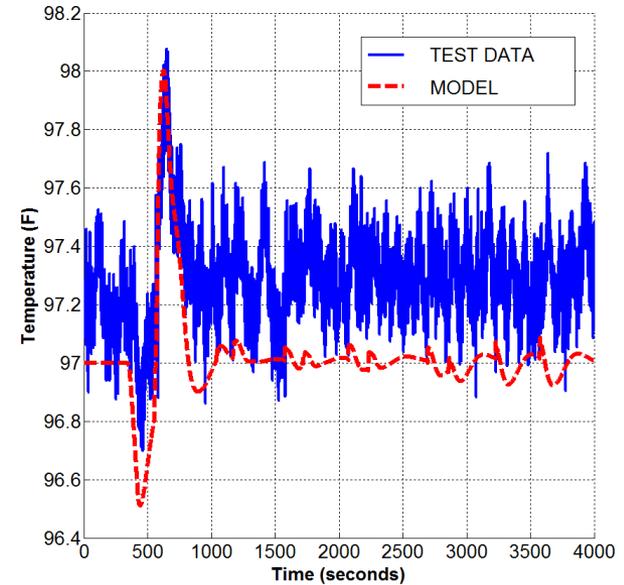
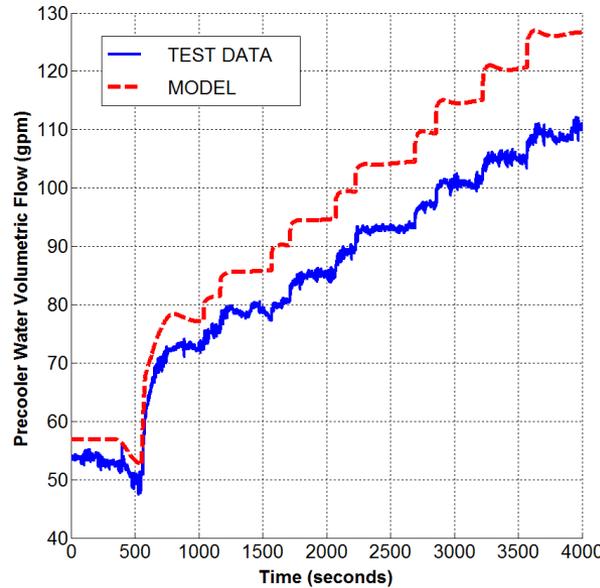
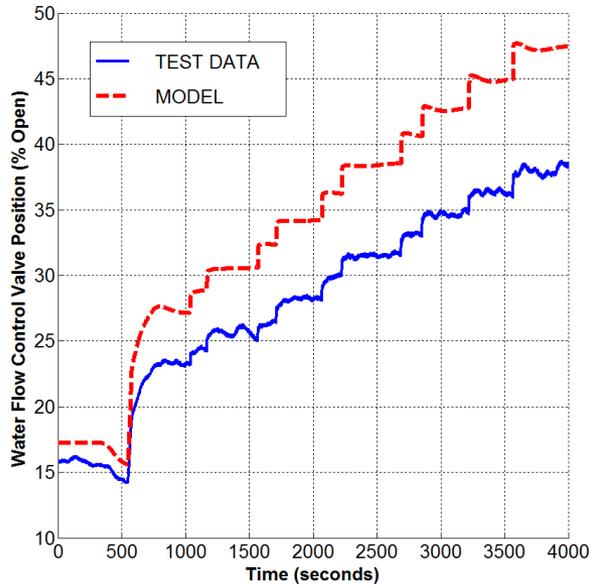
Recirculation Valve Position



# Power Increase Transient: Turbine Generator Power

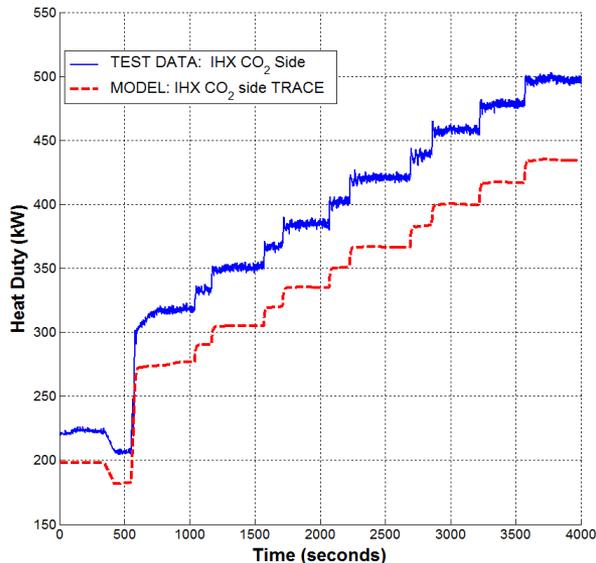
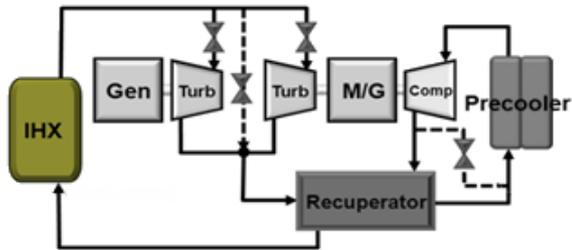


# Power Increase Transient: Cooling Water Control Valve Position, Flow Rate and Compressor Inlet Temperature

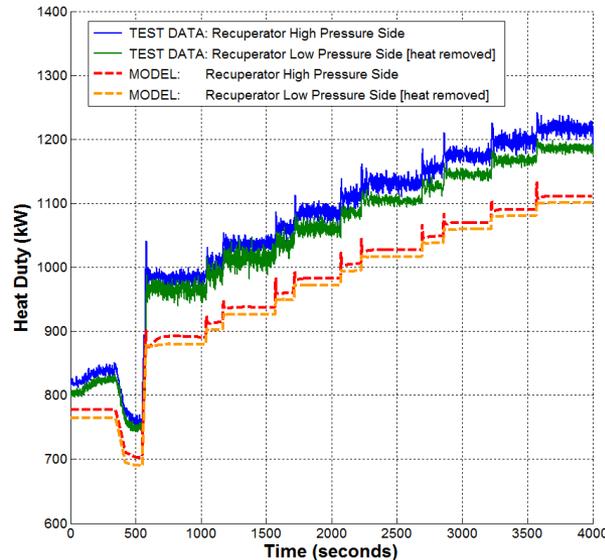
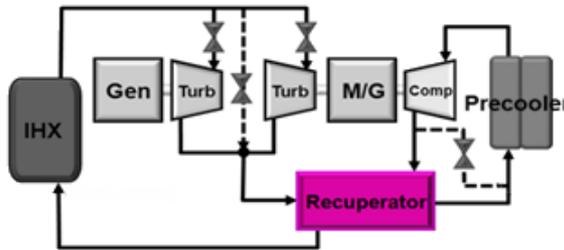


# Power Increase Transient: Heat Exchanger Heat Duties

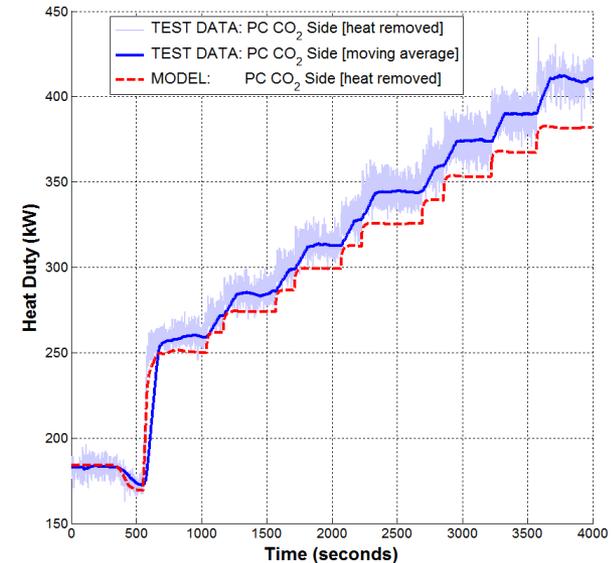
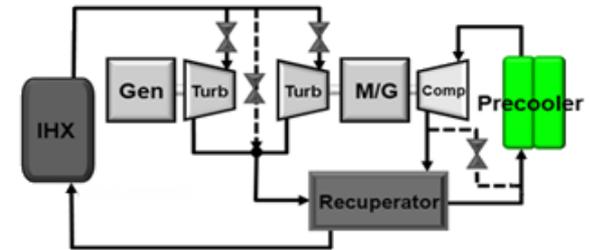
Intermediate Hx



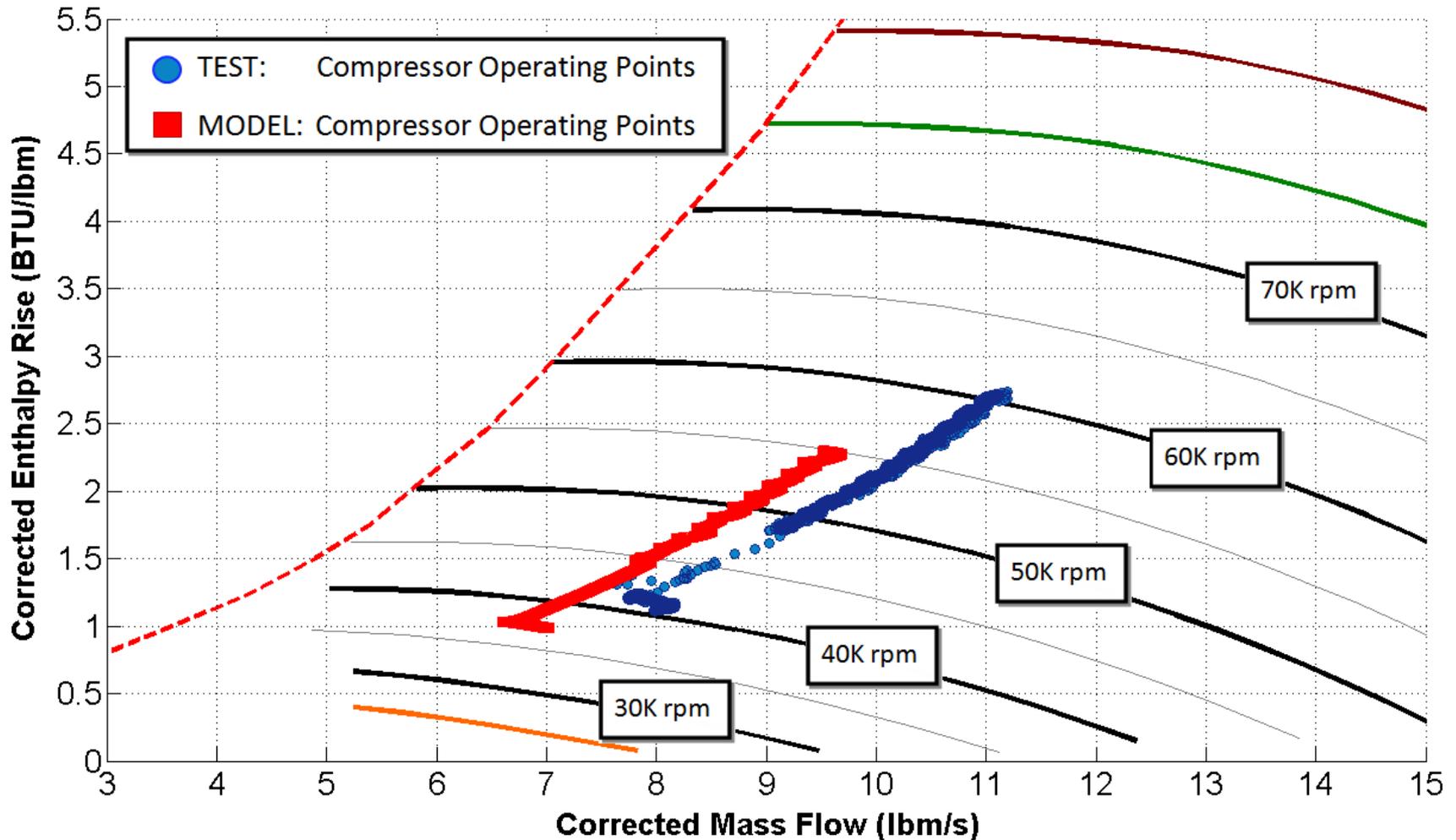
Recuperator



Precooler



# Power Increase Transient: Comparison of Compressor Operation



# Factors that Influence Runtime

- CPU time (clock time) is a function of
  - Computer Hardware (RAM speed, etc.)
  - Model Complexity
    - Component nodalization
    - Fluid property models and interrogation (PG-1<sup>®</sup>, Water, CO<sub>2</sub>, etc.)
  - Transient Rate of Change
    - Heat up/Power Transients/Turbomachinery startup/etc.
  - Model/Physical time: time of actual transient (hour heat up)
  
- Up until now: *Model Time* << *CPU time*
  - *Root cause - largest contributor was fluid property calls*
  
- Now: *Model Time* ≈ *CPU time*
  - *Change is the replacement of NIST property calculations with commercial package (FIT) [Northland Numerics]*

# NIST/FIT Comparison: Benchmarking

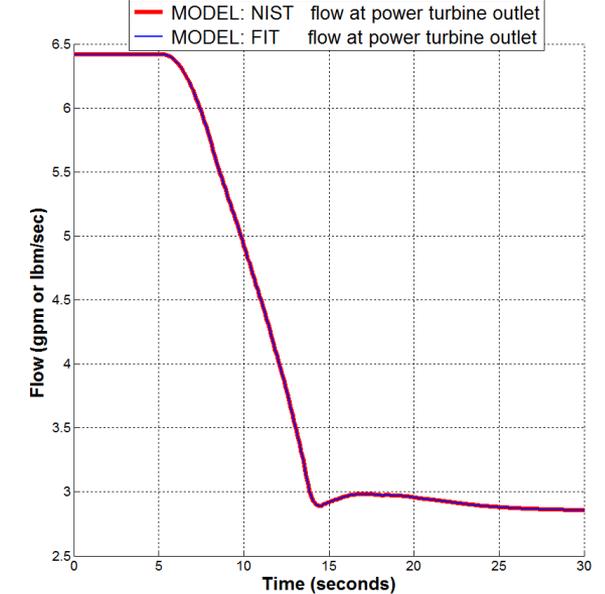
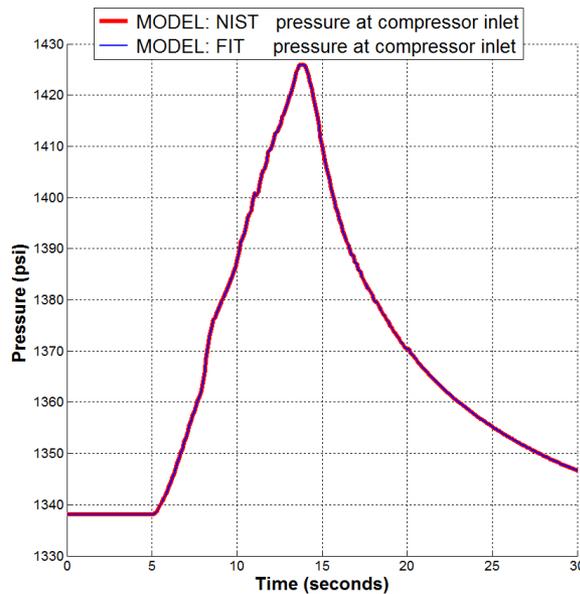
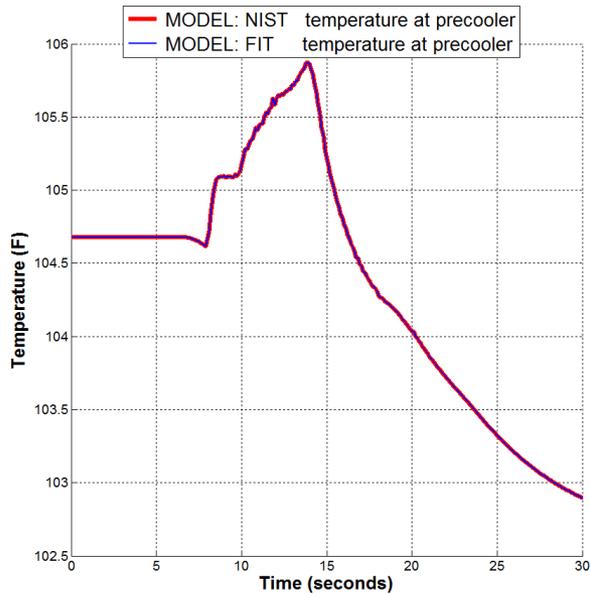
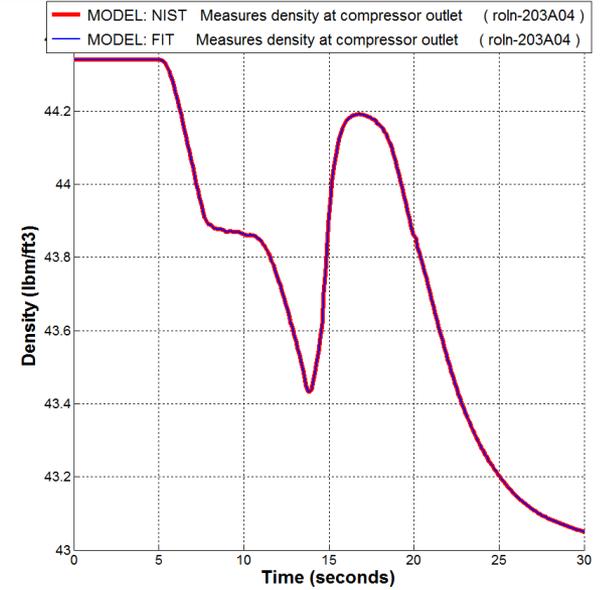
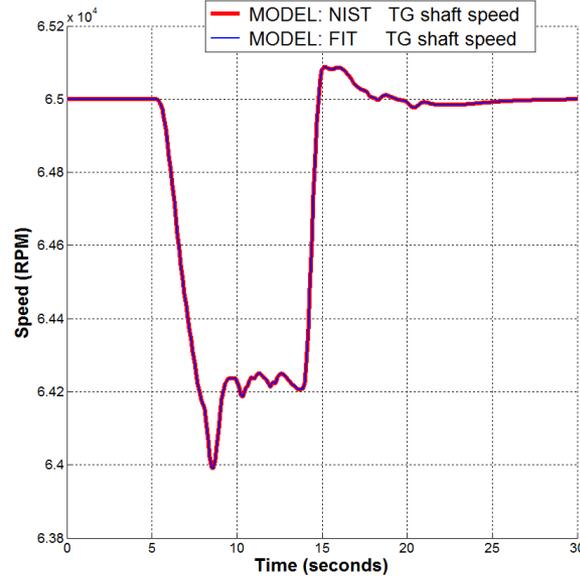
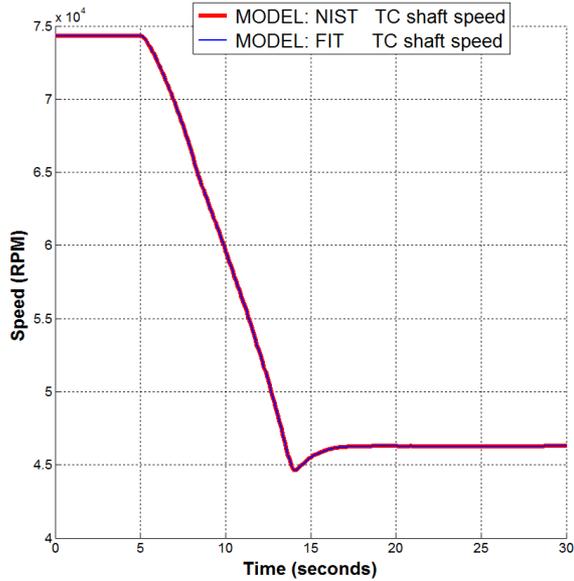
## ➤ Suite of 15 transient runs

- Range in duration from 50 to 4000 seconds (physical time)
- Include entire range of operations
  - Cold (150°F) with both shafts off
  - Start up
  - Configuration of CWS
  - Heat up/Power Transients



Run Name	Run Id	Model Run Description	model time (seconds)	NIST CPU time (seconds)	NIST to Real Time	FIT CPU time (seconds)	FIT to Real Time
<i>IST_v4p017_START_TG65K.med</i>	<i>START</i>	Model startup at full power conditions. Thot = 570F.	50	495	<b>9.91</b>	63	<b>1.26</b>
<i>Rs1ss_THL_TG65K</i>	<i>Restart 1</i>	Reduce TG speed to 65krpm. CCV4 open from 0.00 to 0.06	400	3006	<b>7.51</b>	358	<b>0.90</b>
<i>Rs2ss_Speed_TG65K</i>	<i>Restart 2</i>	Control switches changed to transition from T/H LEAD to SPEED ctrl.	400	3444	<b>8.61</b>	397	<b>0.99</b>
<i>Rs3DP_10pps_MG_TG65K</i>	<i>Restart 3</i>	Down power. Recirculation valve open from 0.06 to 0.59.	400	4126	<b>10.32</b>	461	<b>1.15</b>
<i>Rs4DP_HIdle_CD300_MG_TG65K</i>	<i>Restart 4</i>	TC speed dropped to idle then Thot reduced from 570F to 300F.	3700	31300	<b>8.46</b>	3530	<b>0.95</b>
<i>Rs5_CD150_MG_TG65K</i>	<i>Restart 5</i>	Cool down from 300F to 150F with TC/TG idle.	3700	33377	<b>9.02</b>	3521	<b>0.95</b>
<i>Rs6CWS_OL_lloop_Cidle</i>	<i>Restart 6</i>	Configure CWS to heating mode (isolate inner loop and start Pump1)	400	4777	<b>11.94</b>	510	<b>1.28</b>
<i>Rs7S1S2SD_150F_CWS100F</i>	<i>Restart 7</i>	TC and TG shut down from idle. Turbine inlet T = 150F.	200	2011	<b>10.05</b>	249	<b>1.24</b>
<i>Rs8S1S2SU_150F</i>	<i>Restart 8</i>	TC and TG start up from 0 rpm. Turbine inlet T = 150F.	120	1838	<b>15.31</b>	218	<b>1.82</b>
<i>Rs9lLoopSD_150F</i>	<i>Restart 9</i>	CWS inner loop pump ON to OFF. CWS to cooling config.	240	3044	<b>12.69</b>	353	<b>1.47</b>
<i>Rs10_WCV3auto_Cidle</i>	<i>Restart 10</i>	Transition to cold idle. Comp inlet temp 100F. WCV3 in auto.	1400	13694	<b>9.78</b>	1321	<b>0.94</b>
<i>Rs11HU300F_1Hr_TG65Ktab</i>	<i>Restart 11</i>	Brayton loop heated to 300F from cold idle.	4000	36197	<b>9.05</b>	3790	<b>0.95</b>
<i>Rs12HU435F_1Hr_TG65Ktab</i>	<i>Restart 12</i>	Brayton loop heated to 435F from 300F.	4000	34304	<b>8.58</b>	3786	<b>0.95</b>
<i>Rs13HU540F_1Hr_TG65Ktab</i>	<i>Restart 13</i>	Brayton loop heated to 540F from 435F.	4000	39875	<b>9.97</b>	3852	<b>0.96</b>
<i>Rs14_TCTG55K_540F_TG65Ktab</i>	<i>Restart 14</i>	Raise TC and TG speeds from idle to 55 krpm.	300	3080	<b>10.27</b>	299	<b>1.00</b>

# Transient Comparisons: NIST vs. FIT



# Summary

- TRACE has been demonstrated as an effective tool for S-CO<sub>2</sub> Brayton analysis
  - SNAP GUI/AptPlot enables
    - efficient model building
    - interpretation of results (animation views)
  - predicts loop steady state conditions
  - transient predictions support control system development and operation
  - minimizes risks (trial and error approach) during testing
  
- High fidelity transient modeling on a PC can approach real time execution by replacing NIST REFPROP with Northland Numerics FIT
  
- IST transient model still evolving: as-designed → as-built → as-tested
  - Update performance maps
  - Update windage correlation
  - Update component performance (e.g. valve  $C_{SUBV}$ , Hx's dP)
  
- Future: complete qualification of TRACE code for use as an effective tool for scale-up designs