

# Materials Evaluation and Corrosion Test Needs for a Direct-Fired sCO2 Oxy-Combustion Plant

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#### **Presentation Overview**



- Oxy-Combustion Application
- Overview of Materials
- Existing Test Data & Oxy-Combustion Variables of Interest
- Materials of Interest
  - 400 500 °C
  - 650 750 °C
- Future Test Needs and Recommendations

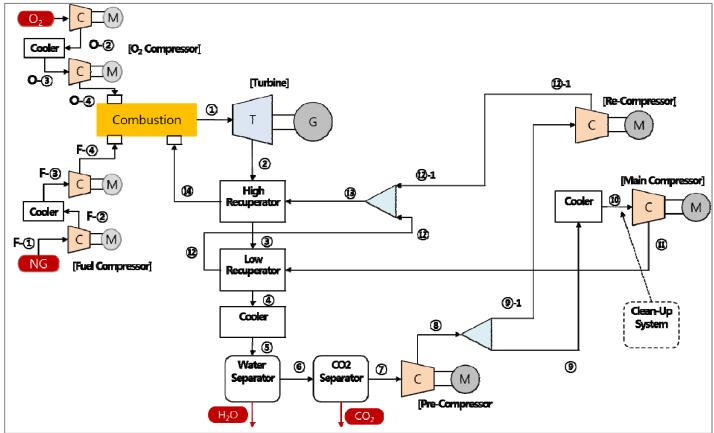
#### **Oxy-Combustion Plant Application**



- sCO2 oxy-combustion cycles have potential for
  - High thermal and plant efficiencies
  - Reduced CO2 emissions
- KEPCO Research Institute leading project to develop an oxycombustion gas turbine power plant
  - Minimize development risk with maximum turbine inlet conditions of 750 °C and 300 bara.
  - Hanwha Power Systems (turbomachinery)
  - Southwest Research Institute (ox-combustor)
  - Other academic Institutions in Korea and U.S.

### What's an Oxy-Combustion sCO<sub>2</sub> Cycle?



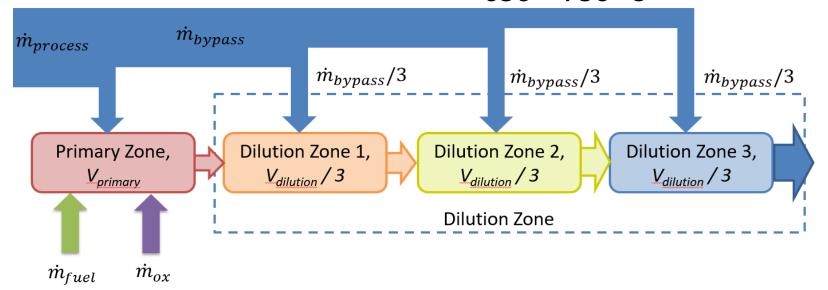


Closed Loop Composition is Affected by Air Separation, Combustion, and Cleanup

#### **Oxy-Combustor Material Needs**



- Combustor pressure vessel at process temperature
- Injector, liner cooled by process but at higher temperatures, lower stress
- $400 500 \,^{\circ}\text{C}$ • Two temperature ranges identified : •  $650 - 750 \,^{\circ}\text{C}$



### Why Focus on Corrosion?



- The majority of metal alloys will corrode.
- Corrosion affects every industry: Infrastructure, Utilities, Transportation, Production & Manufacturing, Government
- Engineering design usually increase corrosion issues.
- Corrosion is **expensive**: estimated between B\$575 (3.1% GDP) to T\$1.1 (6% GDP).

### Materials Deterioration in sCO<sub>2</sub>



#### Corrosion:

- Reaction of metals with oxygen.
- Oxygen comes from:  $CO_2 = 0.5 O_2 + CO$ .
- Growth of oxide film layer.

#### Carburization:

- Cr reacts with C → chromium carbide.
- Carbon penetrate through grain boundary.
- Carburization leads to spalliation of oxide films.

#### **Materials of Interest**



- 5 families of materials:
  - MFSS: martensitic stainless steels (10%-30% Cr) and ferritic stainless steels (12%-17% Cr with 0.15 0.63% C)
  - ASS: austenitic stainless steels (16 to 30% chromium and 2 to 20% nickel).
  - Al SS: alumina oxide austenitic stainless steels.
  - CrNi: chromium nickel alloys.
  - AlNi: alumina oxide nickel alloys.

### **Experimental Methods Summary**



Method	Measure	Pros	Cons
Weight measurement	Oxide film growth	• Easy • Cheap	<ul> <li>No carburization/corrosion product differentiation.</li> <li>Spalliation and material loss affect measurement.</li> </ul>
Micro hardness	Micro hardness Carburization		Coupled with SEM/EDS to confirm carburization
SEM/EDS	Oxide film morphology and composition		
Tensile test	mechanical properties	Environmental effect on mechanical properties	Only after exposure
GENERAL			Lack of in-situ (HTHP problem)

### **Effect of Temperature**



#### Temperature **7** = worsen corrosion, increase carburization

Temperature (°C)	200	250	400	450	F00	FFO	CC0	CEO	700	750	900	050	000
Type of alloy	300	350	400	450	500	550	660	650	700	750	800	850	900
Martensitic & Ferritic													
Austenitic													
Alumina SS													
Chromium Ni													
Alumina Ni													

Based on combination of mass gain, oxide thickness, presence of crack, carburization, etc...:

**Green:** acceptable

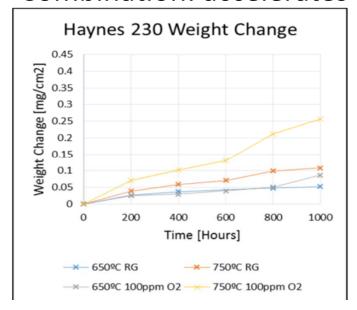
Red: avoid

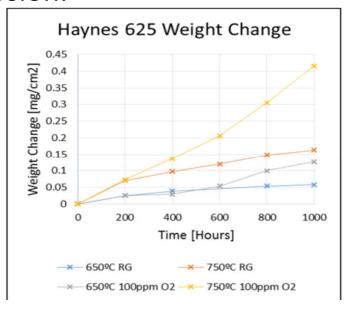
Alumina alloys are not good at low temperature because the alumina oxide does not form fast enough.

## Contamination of sCO<sub>2</sub> with O<sub>2</sub>



- Contamination with O<sub>2</sub>, water, and combination of both.
  - $O_2$ : may be beneficial or detrimental.
  - Water: accelerates corrosion.
  - Combination: accelerates corrosion.



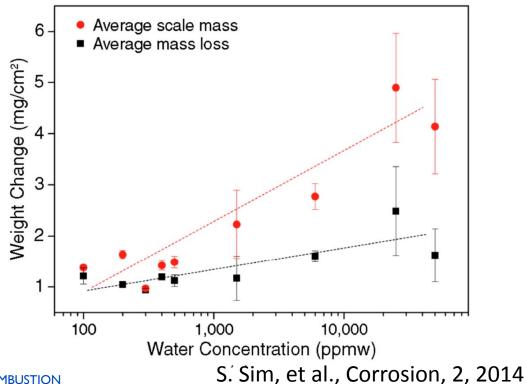


SCO2 MA Mahaffey, J., et al., 5th Symposium on sCO2 Power Cycles, , 2016, Paper #114.

### Contamination of sCO<sub>2</sub> with H<sub>2</sub>O



- Contamination with water accelerates corrosion.
- Impact of water on weight change in sCO<sub>2</sub> at 8 MPa, 40°C.



#### **Coating**



- Thermal barrier coating (TBC) for corrosion protection:
  - Diffusion bond coatings (Pt diffusion or simple or Pt-modified aluminide) with commercially vapor-deposited yttriastabilized zirconia (YSZ) top coatings.
  - High velocity oxygen fuel (HVOF) sprayed MCrAlYHfSi bond coatings with air-plasma sprayed YSZ top coatings.
- Data only at higher temperature (1150°C): failure after 2260 1 hr cycles.
- CO<sub>2</sub> and/or air contamination reduces the time to failure.
- Intrinsic damages: oxide growth, internal stresses leading to cracking and failure.
- Extrinsic damages: erosion, local damages due to impact or particles melting, diffusing, and hardening the top coat leading to potential failure.

# Chosen Materials – <u>400-500°C</u> Combustor Inlet & Pressure Vessel



Trade Name	UNS	Standard Specification	Notes	Max Temperatu Limit [°C] (BPV Code Section)	Allowable Stress at 500°C [MPa]
Gr91	K90901	ASTM A387 Grade 91 Class 2	Reference. Most commonly tested MFSS.	649 (VIII-2)	204
800H	N08800	ASTM B407		816 (VIII-2)	138
310	S31000	ASTM A965		816 (VIII-2)	116
347H/347HF G	S34709	ASTM A965		816 (VIII-2)	125

# Alternative Materials – <u>400-500°C</u> Combustor Inlet & Pressure Vessel



Trade Name	UNS	Standard Specification	Max Temperature Limit [°C] (BPV Code Section)	Allowable Stress at 500°C [MPa]
625	N06625	ASTM B443	593 (I) or 649 (VIII-1)	192
HK40	J94204	ASTM A351	-	-
HK50	J94224	ASTM A297	-	-
310HCbN/HR3C	S31042	ASTM A959	732 (I)	117-158
NF709	S31025	ASTM A213	-	-
HR120	N08120	ASTM B515	899 (VIII-1)	113-153

# **Chosen Materials – <u>650-750°C</u> Combustor Exit & Liner**



Trade Name	UNS	Standard Specs	Max Temperature Limit [°C] (BPV Code Section)	Allowable Stress at 500°C [MPa]	Yield Strength at 750-760°C [MPa]	Creep Rupture Strength at 750°C [MPa] (hr)
740H	N07740	ASTM B983	800 (I)	84.1	596	200 10k)
282	N07208	ASTM B637-12	800 (est.)	105 (est.)	612	186 (10k)
230	N06230	ASTM B572-06	982 (VIII-1)	50.8	323	91-98 (10k)

# Alternative Materials – <u>650-750°C</u> Combustor Exit & Liner

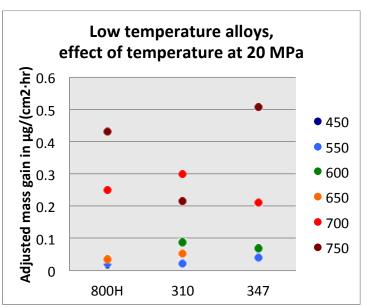


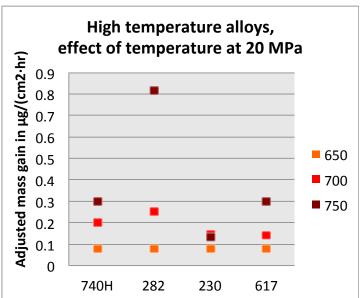
Trade Name	UNS	Standard Specs	Max Temperature Limit [°C] (BPV Code Section)	Allowable Stress at 500°C [MPa]	Yield Strength at 750-760°C [MPa]	Creep Rupture Strength at 750°C [MPa] (hr)
Waspaloy	N07001	ASTM B637	-	-	706	290 (1k)
Udimet 720	N07720	n/a	-	-	770	480 1k)
Rene 41	N07041	SAE AS7469B	-		938	276 (1k)
617	N06617	ASTM B167	982 (VIII-1)	50.4	072	140 (1k)
MA 754	N07754	n/a	-		275	-
Hastelloy X	N06002	ASTM B572-06	482 (VIII-2)	-	218	107 (1k)

# Proposed Materials: Existing Data in sCO<sub>2</sub>, constant pressure.



- Data adjust to mass gain in µg/(cm²·hr) because not all tests are the same duration.
- Increase in mass gain with increase in temperature at 20 MPa.





References:

Cao, G., et al., Corrosion Science, 60, 2012

Jelinek, J.J., et al., NACE Paper C2012-1428

**Lee, H.J., et al.,** 4<sup>th</sup> Symposium on sCO2 Power Cycles, 2014, Paper #32.

Lee, H.J., et al., Corrosion Science, 99, 2015

**Mahaffey, J., et al.,** 5th Symposium on sCO2 Power Cycles, , 2016, Paper #114.

Pint, B.A., Keiser, J.R., 4th Symposium on sCO2 Power Cycles, , 2014, Paper #61

**Pint, B.A., Keiser, J.R.,** JOM, 11, 2015

**Pint, B.A., et al.,** NACE Paper C2016-7747

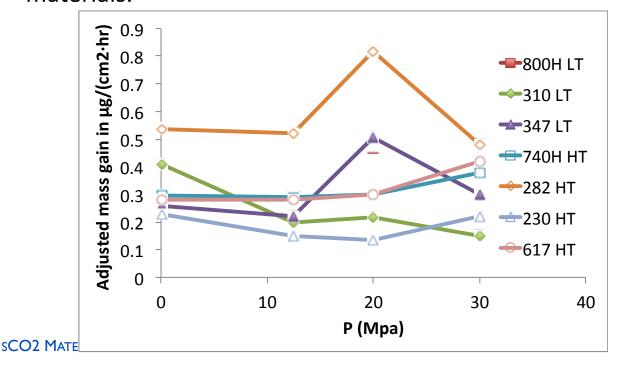
**Pint, B.A., et al.** 5th Symposium on sCO2 Power Cycles, , 2016, Paper #56.

**SCO2 MATERIALS FOR OXY-COMBUSTION** 

# Proposed Materials: Existing Data in sCO<sub>2</sub>, constant temperature.



- No visible trend of mass gain with increase in pressure at 750C.
- High temperature materials had lower mass gain than low temperature materials.



#### **References:**

**Mahaffey, J., et al.,** 5th Symposium on sCO2 Power Cycles, , 2016, Paper #114.

**Pint, B.A., Keiser, J.R.,** 4th Symposium on sCO2 Power Cycles, , 2014, Paper #61

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#### **Test Plan – Variables of Interest**



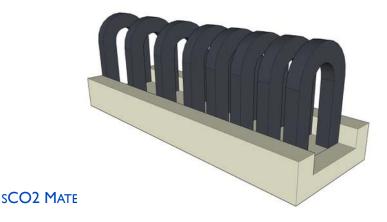
- <u>Temperature</u>: low (combustor inlet) and high (high temperature)
- Pressure: high pressure based on design
- Contamination  $(O_2, H_2O)$ :  $CO_2, H_2O$ , and  $O_2$  mixture matching predicted composition at combustor inlet (low temperature) and exit (high temperature).
- Welding: potential negative impact on the corrosion behavior of chromium-containing alloys

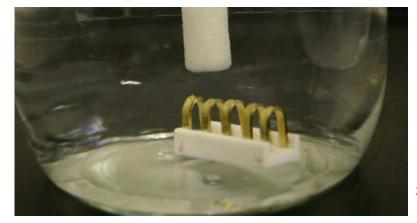
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#### **Test Plan – Variables of Interest**



- <u>Stress corrosion cracking</u>: corrosion combined with stress can lead to early mechanical failure.
- Galvanic corrosion: corrosion may worsen when dissimilar materials are in contact.
- <u>Coating</u>: testing bare and coating materials vapor deposited YSZ, and air-plasma sprayed YSZ.





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#### **Test Plan**



- The recommended tests in O<sub>2</sub>/H<sub>2</sub>O/CO<sub>2</sub> are:
  - High Temp Weight Gain with Tensile Test
  - High Temp C-Ring/U bend
  - Low Temp Weight Gain with Tensile Test
  - High Temp Welding
  - Low Temp C-Ring/U bend
  - Micro hardness
- Statistic: 5 specimens for each test.
- Combine all low temperature and all high temperature.