



# Dynamic modeling and transient analysis of a molten salt heated recompression supercritical CO<sub>2</sub> Brayton cycle

For the 6<sup>th</sup> International Supercritical CO<sub>2</sub> Power Cycles Symposium

Jinyi ZHANG

EDF R&D China

28/03/2018



# OUTLINE

**1.**

**Introduction**

**2.**

**Model Description**

**3.**

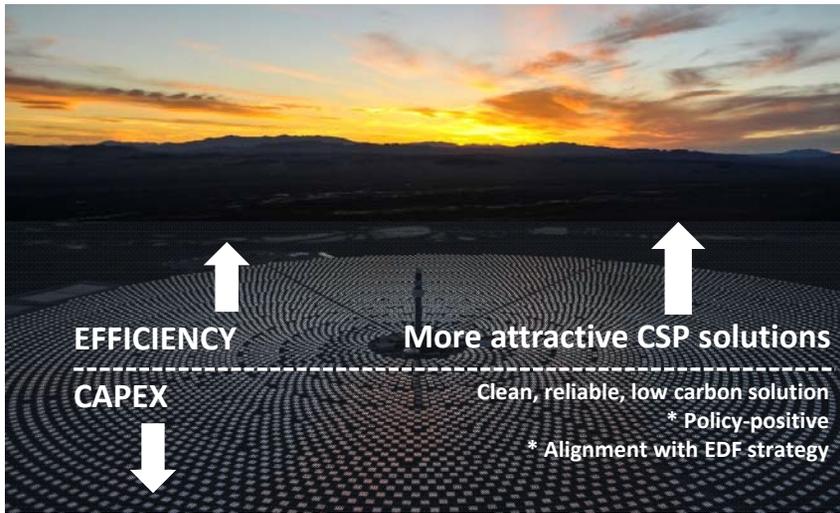
**Part-load control  
strategy and result  
analysis**

**4.**

**Conclusion**

## Introduction

# Supercritical CO<sub>2</sub> Cycle + CSP



- SCO<sub>2</sub>, together with high temperature (> 500 °C) molten salt CSP solutions, could achieve higher efficiency than steam solutions.
- The size of CSP plant is between 50MWe and 150MWe, which is suitable for the first industrial demonstration of cycle.
- Recompression cycle is taken for a preliminary cycle dynamics study, because this is the most studied layout with a good balance between complexity and efficiency.



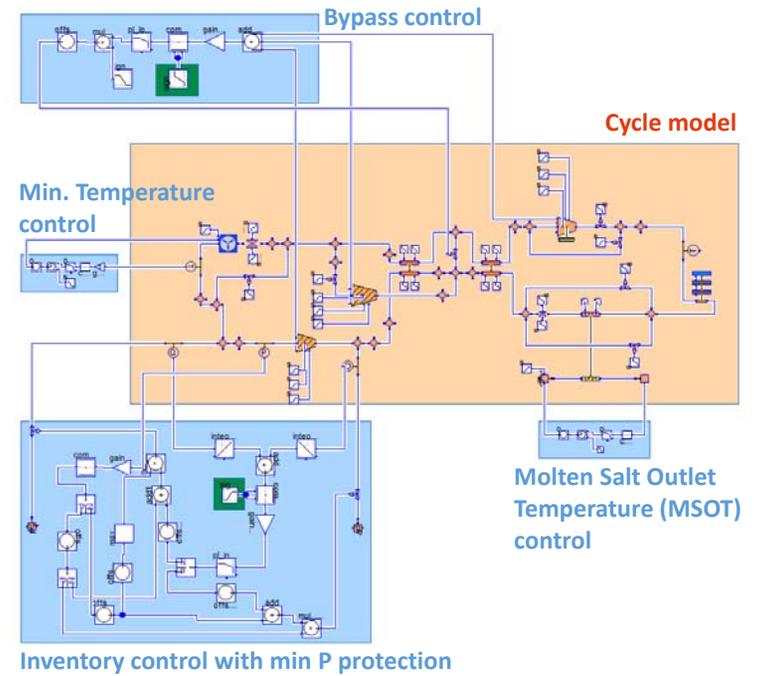
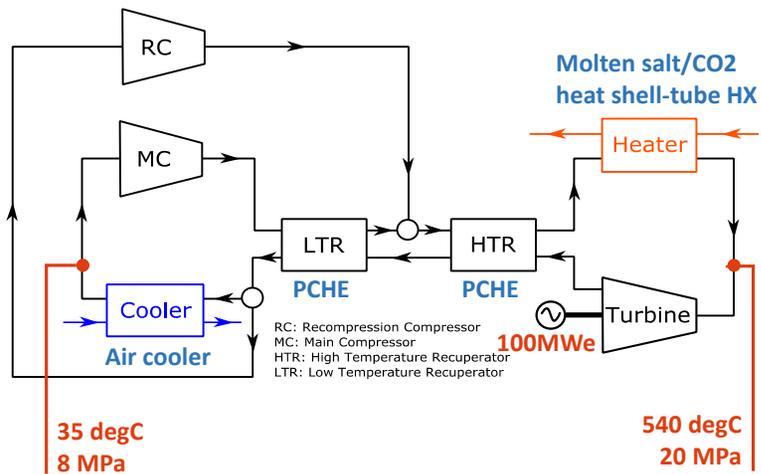
### Design

- **100MWe : average size of CSP plant**
- **Molten salt heated recompression cycle: compatible with current CSP**

## Introduction

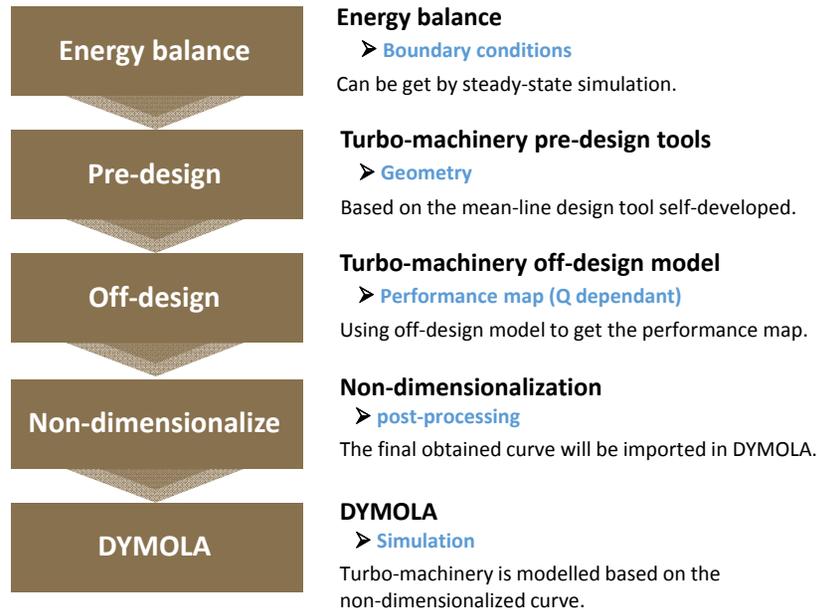
# Dynamic Modeling for Control System Design

Recompression layout



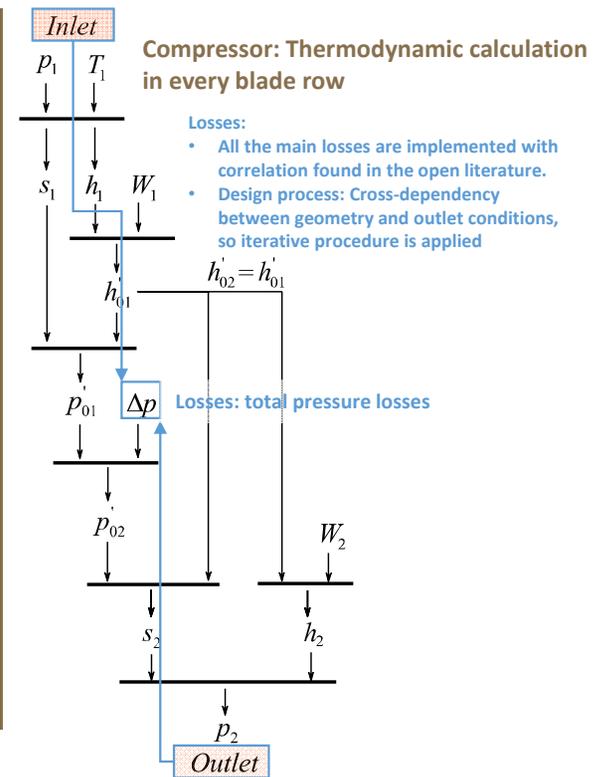
## Model Description

# Turbo-machinery performance model



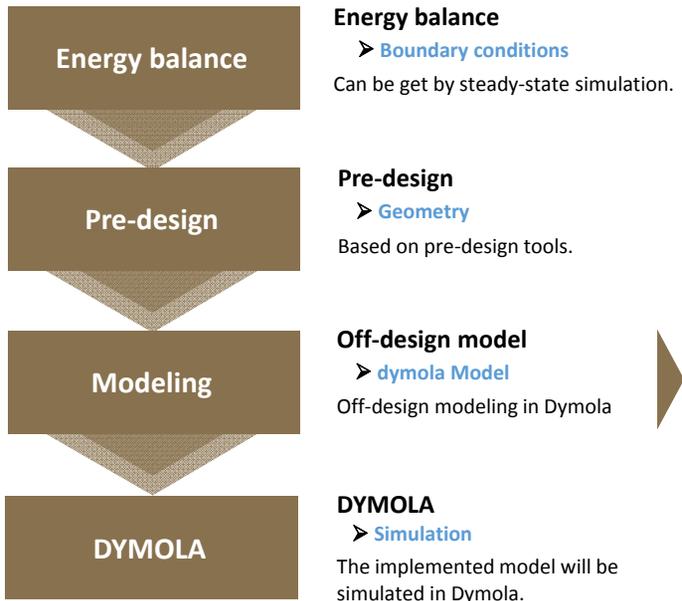
➤➤➤ A realistic model which predicts performance (isentropic efficiency and compression ratio) depending on:

Inlet conditions  
Mass flow rate  
Rotation speed



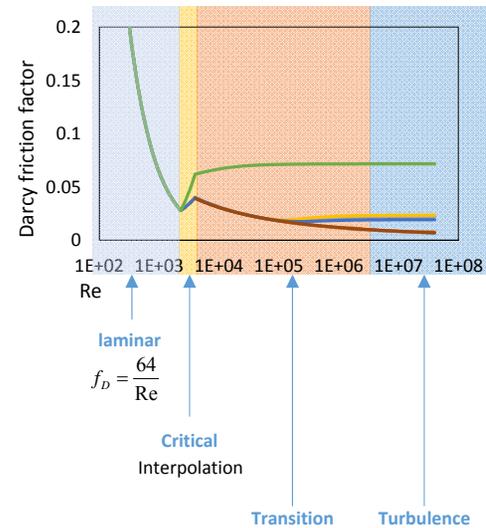
## Model Description

# Heat Exchanger Modeling

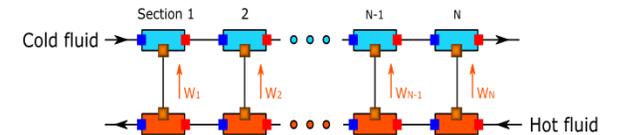


➤➤➤ **A realistic model which predicts on-design and off-design performance of heat exchanger**

Pressure drop: Darcy friction factor



$$\frac{1}{\sqrt{f_D}} = -2 \log_{10} \left( \frac{2.51}{Re \sqrt{f_D}} + \frac{\epsilon}{3.7 D_h} \exp \left( -j \frac{5.66}{Re \sqrt{f_D}} \frac{r}{\epsilon} \right) \right)$$



Heat transfer : Heat transfer coefficient

Laminar flow : Interpolation using following table [Hesselgreaves 2001]

$x^*$	$Nu_{x,H}$		$x^*$	$Nu_{x,H}$	
	D	$\frac{D}{L}$		D	$\frac{D}{L}$
0.000458	17.71	17.43	0.0279	4.767	4.339
0.000954	13.72	13.41	0.0351	4.562	4.037
0.00149	11.80	11.37	0.0442	4.429	3.830
0.00208	10.55	10.08	0.0552	4.276	3.686
0.00271	9.605	9.141	0.0686	4.217	3.543
0.00375	8.475	8.127	0.0849	4.156	3.425
0.00493	7.723	7.375	0.105	4.124	3.330
0.00627	7.137	6.788	0.130	4.118	3.265
0.00777	6.556	6.312	0.159	4.108	3.208
0.00946	6.300	5.912	0.196	—	3.171
0.0128	5.821	5.368	0.241	—	3.161
0.0168	5.396	4.935	0.261	—	3.160
0.0217	5.077	4.579	$\infty$	4.089	3.160

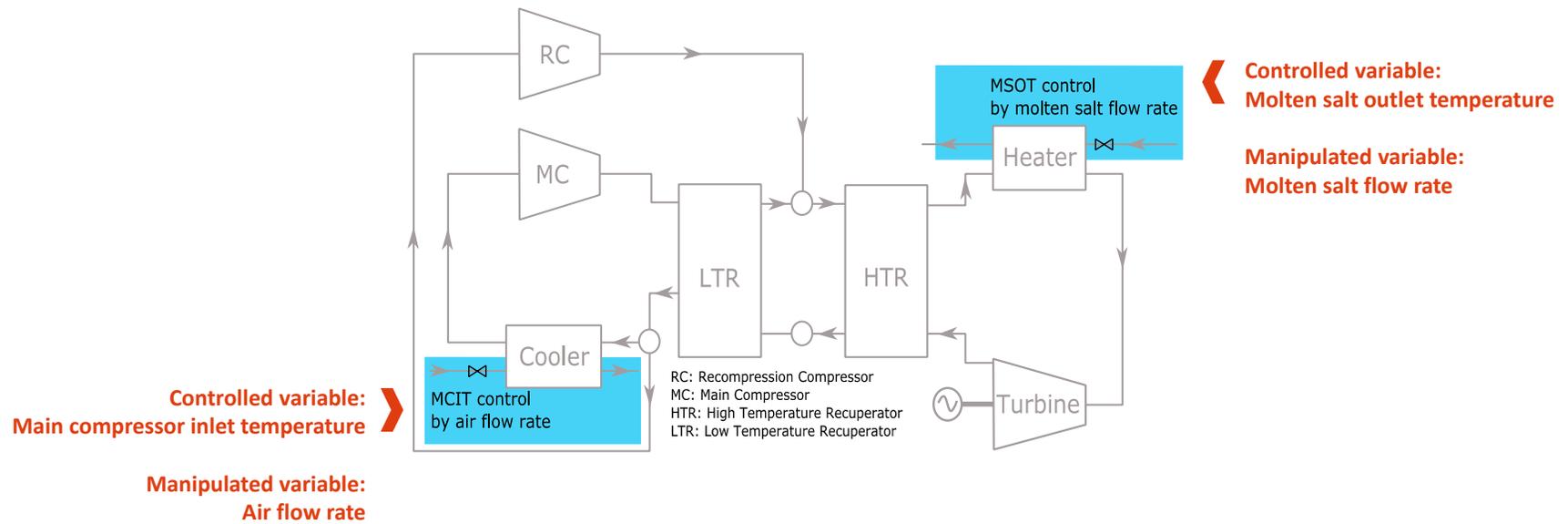
Turbulent flow : Gnielinski Correlation

$$Nu = \frac{(f_D / 8)(Re - 1000) Pr}{1 + 12.7 (f_D / 8)^{1/2} (Pr^{2/3} - 1)} \left( 1 + \left( \frac{D_h}{L} \right)^{2/3} \right)$$

$$\frac{1}{\sqrt{f_{fa}}} = 3.48 - 1.7372 \ln \left( 2 \frac{\epsilon}{D} - \frac{16.2426}{Re} \ln \left( \frac{(2\epsilon / D)^{1.1098}}{6.0983} + \left( \frac{7.149}{Re} \right)^{0.8981} \right) \right)$$

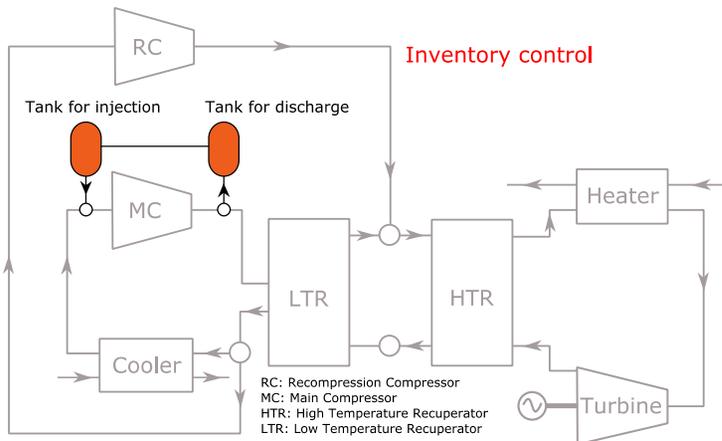
## Model Description

# Basic control loops



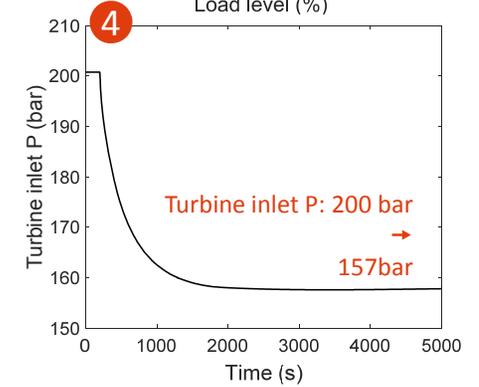
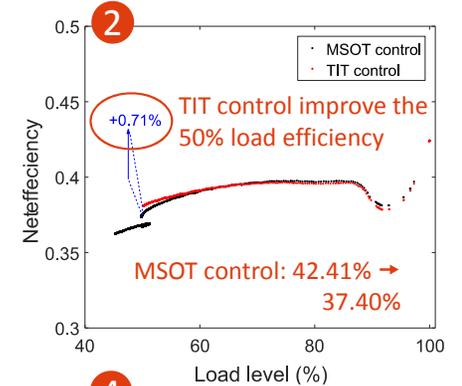
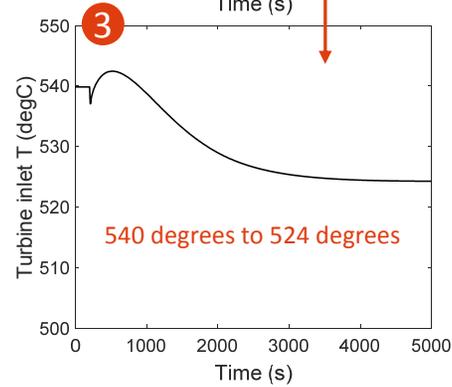
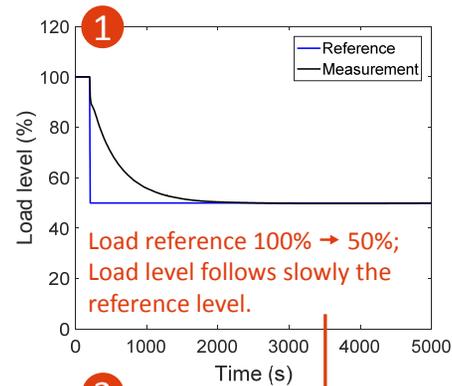
# Part-load Control Strategies and Result Analysis

## Inventory Control



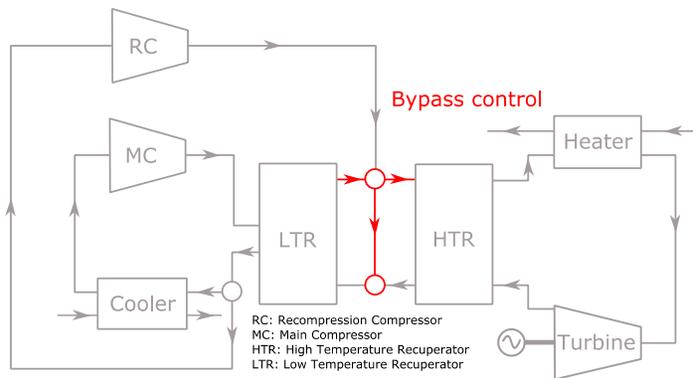
Inventory control with **Main compressor inlet pressure protection**

Pressure protection is important to protect compressor operation.

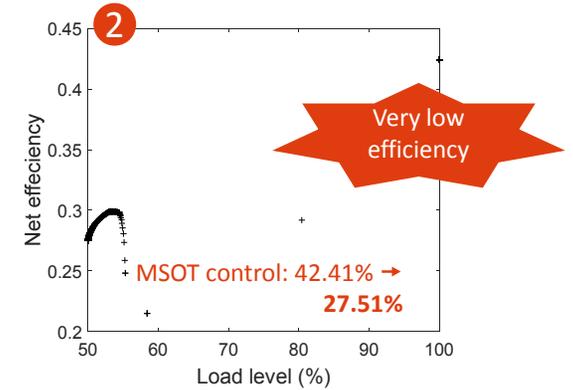
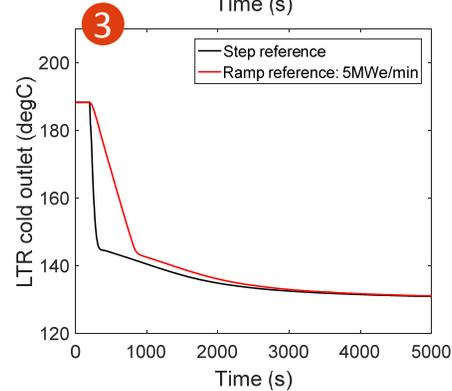
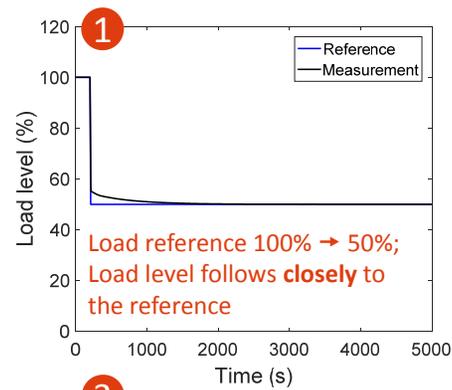


## Part-load Control Strategies and Result Analysis

# Bypass Control



Bypass control: the HTR, heater and turbine are bypassed.



Temperature near PCHEs has a high gradient.

## Part-load Control Strategies and Result Analysis

# Inventory + Bypass Control

### Inventory control

High efficiency  
Low response speed

With Load-inventory table:  
e.g. -50% → 37.2 tons inventory discharge

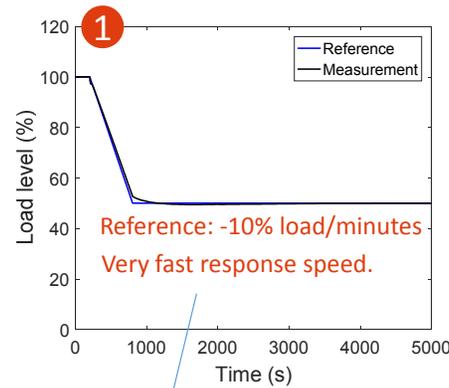


### Bypass control

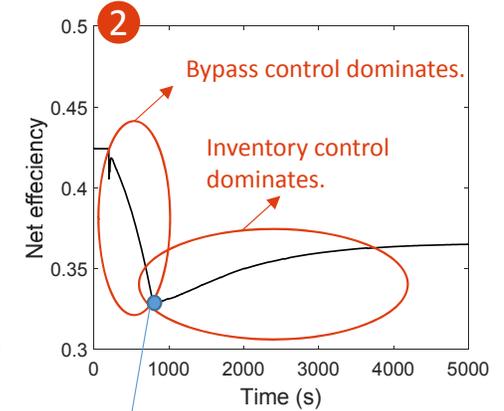
Low efficiency  
High response speed



1. Bypass control and inventory control with load table work together at the beginning of response
2. When inventory control reaches the target amount of inventory discharging, the bypass control will stop.



Higher response time  
Compared to inventory control



Min. efficiency: 32.64%  
Final efficiency: 36.58%

Higher efficiency  
compared to bypass control

## Conclusion

# Perspectives

- A realistic dynamic model of sCO<sub>2</sub> recompression cycle is realized in Dymola.
- Inventory control and bypass control is a good solution for power down, but for **power up**, inventory control is the only choice in the current stage, whose response is not fast;

## Validation and More Control Aspects

- An 20kWth experimental loop is set at the end of 2017, in collaboration with Zhejiang University, which is used to
  - Study pressure drop and heat transfer coefficients
  - Test the cycle dynamics and validate the dynamic model developed for the loop
- Mass management system will be designed to see its impact on inventory control performance;
- Investigate other part-load control strategies, in order to propose an optimized global control strategy with a good **balance between efficiency and response speed** for the whole range of load;
- MSOT and TIT control will be further replaced by a multi-variable control;
- Real-time optimization will be implemented to improve cycle efficiency during operation;

A large industrial tunnel, likely a tunnel boring machine (TBM) cutterhead, with a worker in white overalls and a hard hat lying on the floor at the end. The tunnel is lined with orange metal and has a large yellow circular opening at the far end. The worker is positioned in the center of the tunnel, looking towards the opening.

# Merci

# 谢谢

Contact: [Jinyi.zhang@edf.fr](mailto:Jinyi.zhang@edf.fr)